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TITLE OF THE INVENTION:

AUTOMATIC MECHANICALLY CONTROLLED CONTINUOUSLY-VARIABLE-
RATIO DRIVE

10 The present invention relates to an automatic
mechanically controlled continuously-variable-ratio
drive, particularly for a vehicle.

BACKGROUND OF THE INVENTION

Drives of the above type are known, which
15 substantially comprise an input shaft; and a drive pulley
connectable to the input shaft and comprising two half-
pulleys defining a V groove of variable size to adjust
the winding diameter of a V belt. The pulley is located
between a clutch disk connected rigidly to the input
20 shaft, and a disk-pusher plate angularly integral with
but sliding axially with respect to the input shaft.

In automatic mechanical control solutions, friction
seals are interposed between the half-pulleys and the
clutch disk and disk-pusher plate respectively, and a
25 centrifugal control device cooperates with the disk-
pusher plate to move it axially towards the pulley by an
amount varying as a function of the speed of the shaft.

More specifically, in one known solution, the

control device comprises a hub fixed rigidly to the shaft; and a number of centrifugal weights carried by the hub and for centrifugally exerting axial thrust on the disk-pusher plate, so as first to connect the pulley to the input shaft by means of the friction seals, and then gradually reduce the distance between the half-pulleys as the angular speed of the input shaft increases.

Known drives of the type briefly described above are used widely in low-power motorcycles, in particular scooters, but, though used frequently, have various drawbacks in higher-power applications, such as so-called microcars.

In particular, irregular response of the control device to variations in shaft speed, i.e. to the accelerator, results in "jerking" when accelerating and decelerating, and which is especially noticeable at low engine speed, when starting and parking.

Another drawback of known drives is relatively severe wear of the belt, caused by the belt slipping with respect to the half-pulleys at start-up, when the axial thrust exerted on the half-pulleys by the control device is low.

SUMMARY OF THE INVENTION

It is an object of the present invention to provide a continuously-variable-ratio drive for a vehicle, designed to eliminate the aforementioned drawbacks of known drives.

According to the present invention, there is

provided a drive as claimed in Claim 1.

BRIEF DESCRIPTION OF THE DRAWINGS

A preferred, non-limiting embodiment of the present invention will be described by way of example with
5 reference to the accompanying drawings, in which:

Figure 1 shows a side view of a drive in accordance with the present invention and in a first operating position;

Figure 2 shows an axial section of a drive assembly
10 of the Figure 1 drive, the top and bottom halves of which show two operating conditions;

Figure 3 shows the same axial section as in Figure 2, and the top and bottom halves of which show two operating conditions;

15 Figure 4 shows an axial section of the drive assembly in a different plane from the Figure 2 and 3 sections;

Figure 5 shows a face view of a first component of the drive;

20 Figure 6 shows a view in perspective of the Figure 5 component;

Figure 7 shows a section along line VII-VII in Figure 5;

Figure 8 shows a face view of a second component of
25 the drive;

Figure 9 shows a view in perspective of the Figure 8 component;

Figure 10 shows a section along line X-X in Figure

8.

DETAILED DESCRIPTION OF THE INVENTION

Number 1 in Figure 1 indicates as a whole an automatic mechanically controlled variable-ratio drive for a vehicle, e.g. a scooter or microcar.

Drive 1 comprises an input shaft 2 of axis A; an output shaft 3 of axis B parallel to axis A; a drive assembly 5 fitted to input shaft 2 and having a drive pulley 6 connectable to input shaft 2; and a driven pulley 7 fitted to output shaft 3.

Pulleys 6 and 7 are defined respectively by two half-pulleys 6a, 6b and 7a, 7b defining respective grooves 8 of variable size for a V belt C.

Input shaft 2 is connected rigidly to a flywheel 10 in turn fixed to a drive shaft 12 of an engine 13 (shown partly) of the vehicle.

More specifically (Figures 2 and 3), drive assembly 5 comprises a sleeve 15 fitted idly and with a limited amount of axial slide to input shaft 2. A first half-pulley 6a is fixed rigidly to an end flange 16 of sleeve 15 facing flywheel 10, and is therefore hereinafter referred to as "fixed half-pulley 6a"; and half-pulley 6b (hereinafter referred to as "movable half-pulley 6b") is fitted in axially sliding but angularly fixed manner to sleeve 15, e.g. by a splined coupling 17.

Groove 8 defined by half-pulleys 6a, 6b varies in width alongside variations in the axial position of movable half-pulley 6b, so as to vary the work diameter

of belt C; and axial slide of movable half-pulley 6b along sleeve 15 is limited, in the direction away from fixed half-pulley 6a, by a stop ring 18 on the axial end 19 of sleeve 15 opposite flange 16.

5 Movable half-pulley 6b therefore slides axially between a contact position contacting ring 18 (Figures 1 and 2) and corresponding to the minimum work diameter of belt C, and a maximum-approach position as close as possible to fixed half-pulley 6a (top half of Figure 3)
10 and corresponding to the maximum work diameter of belt C.

 A helical spring 19, externally coaxial with sleeve 15, is compressed axially between half-pulleys 6a and 6b to keep movable half-pulley 6b against ring 18 in the absence of external control thrust. The axial position of
15 ring 18 is selected to keep belt C in contact with both half-pulleys 6a, 6b, with no axial slack, and therefore taut.

 Belt C (Figure 1) transmits motion to driven pulley 7, which is reactive; and half-pulleys 7a, 7b are loaded
20 axially towards each other in known manner by a spring 20, so as to automatically adapt the work diameter in the opposite way to that of pulley 6.

 A clutch disk 24 is fitted in angularly free manner to flange 16 of sleeve 15, is interposed axially between
25 flywheel 10 and fixed half-pulley 6a, and has two peripheral annular friction face seals 25, 26 respectively facing a clutch surface 14 of flywheel 10 and a clutch surface 27 of fixed half-pulley 6a. Clutch

disk 24 is kept permanently contacting clutch surface 27 by an annular spring 28, e.g. with an undulated or cup-shaped profile, interposed axially between clutch disk 24 and a shoulder 29 of flange 16.

5 Clutch disk 24 defines, with clutch surfaces 14 and 27, a friction clutch 32 interposed between flywheel 10 and drive assembly 5.

 Sleeve 15 of drive assembly 5 is supported in rotary and axially free manner on input shaft 2 by means of two
10 bushings 30. Drive assembly 5 is subjected to the axial thrust of a spring 34 surrounding input shaft 2 and compressed between a shoulder 35 of input shaft 2 and drive assembly 5 itself - more specifically, a push ring 33, which slides along input shaft 2 and rests axially
15 against flange 16 of sleeve 15, so as to keep seal 25 of clutch disk 24 detached from clutch surface 14 of flywheel 10. A flange 31 fitted to input shaft 2 defines the limit position of drive assembly 5 produced by spring 34, so that a minimum axial clearance S is defined
20 between seal 25 and clutch surface 14.

 Axial slide of drive assembly 5 on input shaft 2 and of movable half-pulley 6b on sleeve 15 is controlled respectively by an actuating device 42 and a speed adjusting device 43, which together define an automatic
25 mechanical centrifugal control assembly 36 shown in Figures 2 to 4.

 Actuating device 42 comprises a hub 37 fixed rigidly to the end 38 of input shaft 2 opposite flywheel 10. A

free end of hub 37 is fitted with a substantially cup-shaped reaction disk 39 having a conical lateral wall 40 extending towards movable half-pulley 6b so as to surround, and form a cavity 44 with, hub 37.

5 Cavity 44 houses three auxiliary sector-shaped weights 45 (Figures 8, 9, 10) surrounding hub 37 and forming, in pairs, radial gaps 46, one of which is shown in Figure 4. Weights 45 as a whole are shown schematically by the dot-and-dash line in Figure 5. Three
10 radial drive pins 47, projecting from hub 37 and equally spaced 120° apart, engage respective gaps 46 between auxiliary weights 45 to rotate the weights.

Each auxiliary weight 45 is bounded at the end facing drive assembly 5 by a surface 48 sloping
15 substantially 45°, and along the centreline of which is formed a radial recess 49 for the purpose explained later on. On the axially opposite side to surface 48, each auxiliary weight has a peripheral bevel 50 having a conical profile matching the inner profile of lateral
20 wall 40 of reaction disk 39.

Auxiliary weights 45 cooperate with an actuating ring 54, shown in detail in Figures 5, 6 and 7, which is coaxial with hub 37, is loaded by a spring 55 towards auxiliary weights 45, and has a conical end surface 56
25 with a profile matching that of end surfaces 48 of the weights. Three raised radial ribs 57 are formed on surface 56, and engage (Figure 4) respective recesses 49 on auxiliary weights 45 to connect auxiliary weights 45

prismatically to actuating ring 54.

Actuating ring 54 has a friction seal 58 having a conical friction surface 59 facing and tapering the axially opposite way to the auxiliary weights, i.e. towards drive assembly 5.

Friction surface 59 axially faces a matching friction surface 60 formed inside a tubular sleeve 64 projecting axially inside cavity 44 of movable half-pulley 6b and fixed rigidly to movable half-pulley 6b. Sleeve 64 is surrounded by a bushing 74 of soft material, for the purpose explained later on.

Actuating ring 54 defines a push member of actuating device 42, and is subjected to the axial thrust of spring 55 interposed between ring 54 and a plate 63 fixed to input shaft 2. Spring 55 has the dual function of keeping actuating ring 54, and in particular friction surface 59 of seal 58, detached from friction surface 60 of sleeve 64, and of keeping auxiliary weights 45 in a rest position contacting hub 37.

Speed adjusting device 43 comprises an annular push disk 65 fixed rigidly to a back face 66 of movable half-pulley 6b facing reaction disk 39; and push disk 65, conveniently made of pressed sheet metal, has a conical end wall 67 facing conical wall 40 of reaction disk 39, and having the same but opposite taper to that of wall 40.

Speed adjusting device 43 also comprises a number of, e.g. three, main weights 68 housed between walls 40

and 67 and equally spaced angularly about sleeve 64. Weights 68 have a section substantially in the form of an outwardly tapering isosceles trapezium, and are each bounded axially by two end surfaces 70 and 71
5 respectively facing walls 67 and 40.

Weights 68 (Figure 4) are secured, to rotate with and slide radially with respect to movable half-pulley 6b, by respective guide tongues 73 fixed to and projecting axially from movable half-pulley 6b so as to
10 engage respective guide grooves 75 formed in end surfaces 70 of weights 68.

Weights 68 are also secured elastically to movable half-pulley 6b by respective pairs of pull springs 62, which exert on weights 68 inward radial pull to keep them
15 radially contacting bushing 74, and axial pull towards wall 67 of push disk 65 to prevent undesired contact between weights 68 and wall 40 of reaction disk 39.

Drive 1 operates as follows.

When the engine is idling (top half of Figure 2),
20 spring 34 keeps drive assembly 5 in a release position releasing friction clutch 32, i.e. with sleeve 15 resting axially against stop ring 31, and clutch disk 24 detached from flywheel 10.

Actuating device 42 rotates with input shaft 2.
25 Auxiliary weights 45 are maintained in a radially withdrawn position, contacting hub 37, by actuating ring 54, which in turn is pushed axially by spring 55 against auxiliary weights 45, so that friction surface 59 of

friction seal 58 is detached from friction surface 60 of sleeve 64.

Drive assembly 5 therefore does not rotate, and, with it, adjusting device 43 also remains stationary, with main weights 68 held in the radially withdrawn position contacting bush 74 and detached from reaction disk 39 by springs 62.

Spring 19 keeps pulley 6 in the minimum belt C work diameter condition.

As engine speed increases and reaches a predetermined threshold speed, e.g. 1200-1400 rpm, the centrifugal force of auxiliary weights 45 of actuating device 42 overcomes the elastic reaction of spring 55, and auxiliary weights 45 move radially outwards and move actuating ring 54 axially towards drive assembly 5 by the combined effect of the conical coupling of bevels 50 of weights 45 and conical wall 40 of reaction disk 39, and the conical coupling of end surfaces 48 of weights 45 and surface 56 of actuating ring 54. The engine speed at which actuating device 42 kicks in may be selected by appropriately sizing auxiliary weights 45 and spring 55.

Once the initial axial clearance is recovered, friction surface 59 of friction seal 58 on actuating ring 54 cooperates with friction surface 60 of sleeve 64 to exert axial thrust on the whole of drive assembly 5 towards flywheel 10 and in opposition to the elastic reaction of spring 34.

The axial movement of drive assembly 5 eliminates

the original axial clearance S between clutch disk 24 and clutch surface 14 of flywheel 10 (bottom half of Figure 2), so that drive assembly 5 is made integral with flywheel 10, and therefore with input shaft 2, and main weights 68 are rotated together with drive assembly 5.

In response to a further increase in engine speed, main weights 68 overcome the elastic force of springs 62 and begin to move radially outwards. Once the clearance is taken up, end surfaces 70, 71 of weights 68 exert thrust on conical wall 67 of push disk 65 and conical wall 40 of reaction disk 39. Since reaction disk 39 is fixed axially, further centrifugal radial movement of weights 68 produces an axial movement of push disk 65, and therefore of movable half-pulley 6b towards fixed half-pulley 6a, in opposition to the elastic thrust of spring 19, thus gradually reducing the width of groove 8 and increasing the work diameter of belt C (top half of Figure 3).

When engine speed is reduced, the above operating steps are performed in reverse order. Bushing 74 of soft material provides for deadening the noise produced by main weights 68 being pulled to a stop by springs 62.

The advantages of drive 1 according to the present invention will be clear from the foregoing description.

In particular, using a centrifugal actuating device 42 for rotating drive assembly 5 over a first rotation speed threshold of input shaft 2, and a centrifugal speed adjusting device 43 for adjusting the work diameter of

drive pulley 6 at higher rotation speeds of input shaft 2, provides for smooth, gradual torque transmission, with substantially no irregularity, even in low engine speed transient states, so that starting and parking the
5 vehicle are much smoother and more gradual.

Moreover, by keeping belt C taut at all times, even in the minimum work diameter condition, and preventing half-pulleys 6a, 6b from rotating with respect to each other, there is substantially no slippage of the belt
10 with respect to drive pulley 6 when starting, thus reducing wear of the belt.

Clearly, changes may be made to drive 1 as described herein without, however, departing from the scope of the accompanying Claims.